

1 **Effect of drying and extrusion processing on physical and nutritional**
2 **characteristics of bilberry press cake extrudates**

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12 **Abstract**

13 Mild drying and extrusion processing of side streams from berry juice production can enable retention
14 of valuable compounds in the food chain and reduce waste production. The aim of this study was to
15 evaluate the applicability of using hot air (HA) and microwave assisted hot air (MWAH) drying
16 combined with extrusion for conversion of bilberry press cake into value-added extruded food products.
17 Bilberry press cake was dried at 40 °C by HA and MWAH drying to a moisture content of 17g/100 g.
18 A twin screw extruder (average feed rate 72 g/min, temperature profile 135-128-89-69 °C) was used to
19 extrude products containing organic wholegrain rye flour and 10 % or 25 % dried bilberry press cake
20 powder. A consumer panel (n=15) evaluated four extrudates on hedonic and Just-About-Right (JAR)
21 scales, with a main focus on texture properties. The results indicate that different drying techniques
22 implied a difference in processing time (40 % reduction with MWAH drying). However, the retention
23 of total phenolics and physical characteristics of extruded snacks containing bilberry powders were
24 independent of drying techniques. In sum, powder of bilberry press cake can be incorporated in cereal
25 based extruded snacks with enhanced phenolic content and potential for palatable sensory properties.

26 **1. Introduction**

27 Berries are perishable seasonal products and the shelf-life of fresh berries is normally short. In general,
28 half of fresh fruit and vegetable production is lost before consumption (Gustavsson & Stage, 2011). To
29 increase the commercial value and reduce waste it is reasonable to process berries into more stable
30 products. Drying is a commonly used preservation method for fruits and vegetables, enabling extended
31 shelf life as well as formulation of fruit and vegetable based products (Jangam, Law & Mujumdar, 2010).
32 In the juice industry, the press cake left after juice extraction may account for approximately 30 g/100
33 g of the dry solids of the berries (Kryeviciute, Kraujalis & Venkutonis, 2016). Hence, the side streams
34 from berry juice production may be upgraded into value-added products to achieve sustainable
35 production chains. Grzelak-Blaszczyk, Karlinska, Grzeda, Roj & Kolodziejczyk (2017) studied
36 utilization of strawberry press cake and concluded that it can be used as a food additive high in protein,
37 fibre and polyphenol content which contributes to improved sustainability of the fruit industry.
38 Bilberries (*Vaccinium myrtillus* L.), wild growing berries in northern Europe and North America, are
39 naturally rich in polyphenols such as anthocyanins (Mikulic-Petkovsek, Schmitzer, Slatnar, Stampar &
40 Veberic, 2015) which have been reported to contribute to prevention of a number of diseases such as
41 type 2 diabetes and cardiovascular diseases (Pojer, Mattivi, Johnson & Stockley, 2013). After
42 extraction, the press cake is composed of mainly skins and seed and with them a large part (58 g/100 g
43) of the phenolic compounds present in the berries (Dinkova et al., 2012). Dried press cakes from juice
44 production also contains dietary fibre (ca 68 g/100 g), protein (ca 15 g/100 g) and lipids (Struck, Plaza,
45 Turner & Rohm, 2016). Berries and berry press cake can be dried and milled into stable and convenient
46 powder products, which can be further used as ingredients in the food industry (Figuerola, 2007), such
47 as in extruded snacks and cereals. The addition of bilberry press cake to extruded cereals and snacks
48 brings added flavour as well as higher nutritional value, as the majority of the existing extruded snacks
49 on the market have high carbohydrate, sugar and lipid content and poor nutritional value.

50 The choice of processing methods and conditions has large impact on the characteristics of fruit and
51 vegetable products such as microstructure, flavour and micronutrient retention, textural properties etc
52 (Van Buggenhout et al., 2012). Hot air (HA) drying is a technique commonly used for berry

53 preservation. Microwave assisted hot air (MWHHA) drying, on the other hand, uses microwaves together
54 with hot air to increase drying efficiency and decrease drying time. The drying mechanism is different
55 from HA drying since the microwaves penetrate the product and create internal temperature increase.
56 The latter may affect the microstructure of the dried products and hence, flavour and micronutrient
57 retention. Drying processes using different methods have previously been reported to have significant
58 effects on the degradation of bioactive compounds in berries (Zielinska & Michalska, 2016). Dried berry
59 materials may be further used as food ingredients in for example extruded products. Extrusion
60 processing is a continuous short time high shearing technology, which consists of subsequent series of
61 mixing, forming, puffing and drying processes. It is a useful tool to design expanded ready-to-eat foods
62 (snacks, cereals, etc.) or to modify food ingredients. The extrusion process leads to irreversible changes
63 such as denaturation of proteins and formation of starch-lipid, protein-lipid and protein-protein
64 complexes (Sozer & Poutanen, 2013). The aim of this study was to evaluate the applicability of pre-
65 treatments using HA and MWHHA drying combined with extrusion for conversion of bilberry press cake
66 into value-added extruded food products.

67 **2. Materials and Methods**

68 **2.1.Raw material**

69 Bilberry (*Vaccinium myrtillus* L.) press cake, produced by cold pressing without enzymatic
70 treatment, was supplied by Kalix Syltfabrik AB (Kalix, Sweden). The bilberry press cake contained skin
71 and seeds and had a moisture content of 75.6g/100 g \pm 0.5g/100 g, and was stored in the dark at -40 °C
72 until use. The press cake was thawed in closed, opaque containers at 20 °C overnight (15 h) prior to
73 drying.

74 **2.2. Drying and milling**

75 Bilberry press cake was dried at 40 °C in the absence of light by HA drying and MWHHA drying to a
76 moisture content of 17 g/100 g. The target moisture content of 17 g/ 100 g was chosen to achieve a
77 powder that was dry enough to be included in an extrusion formula, but at the same time the drying time
78 was kept as short as possible to limit energy consumption in a manufacturing process and avoid

79 extensive losses of phenolic compounds and aroma. After drying, the material was stored in sealed
80 polyamide/polyethylene plastic pouches in the dark at -40 °C until milling. In order to obtain enough
81 dried material for extrusion trials HA and MWAHA drying was carried out in two batches, conducted on
82 two subsequent days. After drying, the batches were mixed before milling. The HA drying was realized
83 in a conventional hot air oven (Garomat 142 Electrolux, Stockholm, Sweden), where two trays (size 21
84 x 30 cm) with approximately 1250 g bilberry press cake in each were placed in the middle of the oven.
85 The fan of the oven created an air velocity of 6.1 m/s. The MWAHA drying was performed according to
86 the procedure and system described by Kerbstadt et al. (2015). In brief, 1250 g bilberry press cake was
87 loaded in the microwave cavity (TIVOX Automation AN, Tidaholm, Sweden) that was connected to an
88 air heating unit with a fan (HONEYWELL INU control AB, Borås, Sweden) resulting in an air speed
89 of 0.8 m/s in the middle of the cavity. The microwave power, of maximum 1000 W, was supplied by
90 Magdrive-1400 (Tivox, Tidaholm, Sweden), with wavelength of approximately 0.12 m at a frequency
91 of 2450 MHz. To keep the desired treatment temperature, the microwave power was regulated
92 automatically by the software MagDrive c3.1 (Tivox Maskin AB, Tidaholm, Sweden) dependent on the
93 sample temperature that was measured by fibre optic temperature probes (Neoptix Inc., Quebec,
94 Canada). The dried press cake was milled using a coffee mill (Ascaso i-I, Ascaso, Barcelona, Spain).
95 The milled material was stored in sealed polyamide/polyethylene pouches in the dark at -40°C until
96 further analysis or shipment to the sites for micronutrient analysis or extrusion.

97 **2.3. Moisture content, water activity and particle size distribution**

98 Moisture content of bilberry press cake, dried material, and dried and milled material were measured
99 gravimetrically in a vacuum oven (Sanyo Gallenkamp, Loughborough, UK). The analysis was done in
100 triplicates by drying of approx. 2.5 g sample at 80 °C and 900 mbar in aluminum dishes until constant
101 weight. The water activity was measured in triplicates using an Aqua Lab 4TE (Decagon Devices,
102 Pullman, Washington, USA). Determination of the particle size distribution of the powder was done by
103 a vibratory sieve-shaker (Analysette 3, FRITSCH, Idar-Oberstein, Germany) with sieves of mesh sizes
104 250 µm, 500 µm, 710 µm and 1250 µm. The sieve shaking was run for 10 min at an amplitude of 1.5

105 mm and with an interval of 10 s. Particle size analysis was done in duplicate with about 20 g of powder
106 each time.

107 **2.4. Extrusion**

108 Extruded puffs were prepared by substituting organic wholegrain rye flour (Fazer Mills, Finland) with
109 10 % and 25 % bilberry press cake powders. A reference extruded puff was prepared by using only
110 organic wholegrain rye flour. A twin screw extruder (APV MPF 19/25, Baker Perkins Group Ltd,
111 Peterborough, UK) with an average feed rate of 72 g/min and temperature profile of 135-128-89-69 °C
112 was used, together with a co-rotating twin screw feeder (K-Tron Soder, Niederlenz, Switzerland). The
113 die diameter and screw speed were 3 mm and 360 rpm for all extrusion trials. Water feed rate was set to
114 3.7 g/min only for wholegrain rye flour and the rest of samples were extruded without any water addition
115 as the *in situ* moisture content of berry powder was sufficient for extrusion processing. The moisture
116 content of the feed materials were 11±0.07 g/100 g, 11.6±0.02 g/100 g and 12.5±0.01 g/100 g, for
117 organic wholegrain rye flour , wholegrain rye flour supplemented with 10 % and 25 % billberry press
118 cake powder, respectively. Specific mechanical energy (SME) is an important process parameter used
119 to describe processing conditions and was calculated with Eq. 1

120 (Hu, Hsieh & Huff, 1993):

$$SME \left(\frac{kWh}{kg} \right) = \frac{w}{w_r} * \frac{T}{100} * \frac{Z_r}{Q} \quad (1)$$

121

122 where ω is the screw speed (in rotations per minute, rpm), ω_r is the maximum screw speed of the extruder
123 used (500 rpm), τ is the torque (in percent), Z_r is the maximum power capacity of the extruder (2 kW)
124 and Q is the feed rate (in kilogram per hour). Extruded products were collected continuously from the
125 die exit after manually cutting to a 20 cm length with scissors and dried immediately in an oven for 10
126 min at 100 °C. Extrusion processing was performed in duplicate.

127 **2.5. Stereomicroscopy**

128 For the stereomicroscope imaging of the radial cross-sections of the extrudates, the samples were cut
129 into 10 mm pieces with an electric saw (Power ST-WBS800, Taiwan Sheng Tsai Industrial Co. Ltd.,
130 Taiwan) and examined under a SteREO Discovery.V8 stereomicroscope with an Achromat S 0.5×
131 objective (Carl Zeiss MicroImaging GmbH, Göttingen, Germany) and imaged using a DP-25 single chip
132 colour CCD camera (Olympus Life Science Europa GmbH, Hamburg, Germany) and the Cell^P imaging
133 software (Olympus).

134 **2.6. Macrostructural analysis**

135 Length and diameter in three different points of each sample were measured using a vernier caliper and
136 the average diameters of the samples were obtained. The measurements were made from 20 replicates
137 from each extrusion treatments using the method described by Alam et al. (2014).

138 Expansion rate was calculated with Eq. 2:

$$\text{Expansion rate (\%)} = \frac{D_e}{D_d} \times 100\% \quad (2)$$

139 Where D_e is the average diameter measured at three different points of the extrudate sample (mm) and
140 D_d is the diameter of the die (3 mm).

141 Specific length was calculated with Eq. 3:

$$\text{Specific length (m/kg)} = \frac{L_e}{m_e} \quad (3)$$

142 Where L_e is the length of the extrudate sample (m) and m_e is the mass of the sample (kg). Piece density
143 was calculated with Eq. 4:

$$Piece\ density\ (kg/m^3) = \frac{4 \times m_e}{\pi \times (D_e)^2 \times L_e} \quad (4)$$

144 Where m_e is the mass of the sample (kg), D_e is the average diameter measured at three different points
 145 of the extrudate sample (m) and L_e is the length of the extrudate sample (m).

146 **2.7. Textural properties**

147 Mechanical properties of extrudates were analysed by uniaxial compression test using a texture analyser
 148 (Texture Analyser TA-HDi, HD3071, Stable Micro Systems, United Kingdom) equipped with a 30 kg
 149 load cell and a cylindrical 36 mm aluminium probe. Samples of 10 mm length were cut and equilibrated
 150 at a relative humidity (RH) of 43 % at 21 °C. The samples were deformed at 70 % strain with a test
 151 speed of 1 mm/s. The force-deformation (f-d) curve was obtained to assess the mechanical
 152 characteristics of the extrudate samples. Each measurement was performed with 20 replicates. Texture
 153 Exponent software v.5.1.2.0 (Stable Micro Systems, UK) was used to obtain values of actual and
 154 smoothed curve length, area under the f-d curve (A), number of peaks, crushing force (A / distance of
 155 compression) and hardness (F_{max}). Different approaches were used to describe the crispiness of
 156 extrudates, such as crispiness work (C_w , Eq. 5) and crispiness index (C_i , Eq. 6). High crispiness was
 157 accompanied by low C_w and high C_i value, whereas low crispiness corresponded to high C_w and low
 158 C_i value (Alam et al., 2014; Sibakov et al., 2015).

159

160 Crispiness work was calculated with Eq. 5 (Van Hecke, Allaf & Bouvier, 1998):

$$C_w\ (N\ mm) = \frac{A}{N} \quad 5$$

161 where A is the area under the f-d curve (N mm) and N is the number of peaks.

162 Crispiness index was calculated with Eq. 6 (Heidenreich, Jaros, Rohm & Ziemis, 2004):

$$C_i = \frac{L_N}{A \times F_{mean}} \quad (2)\ 6$$

163 Where L_N is the normalized curve length (length of actual curve/ F_{max}), A is the area under the f-d
 164 curve (N mm) and F_{mean} is the sum of the actual force values divided by the number of peaks (N).

165 **2.8. Dietary fibre analysis of extrudates**

166 Insoluble, soluble and total dietary fibre contents of extrudates were determined according to Megazyme
167 rapid integrated total dietary fibre assay procedure (K-RINTDF 09/16 Megazyme, Ireland) combining
168 key attributes of AOAC Official Methods 2002.02, 985.29, 991.43 and 2001.03. Duplicate test portions
169 of each sample (1 g) were incubated with pancreatic α -amylase (PAA) and amyloglucosidase (AMG)
170 for 4 h at 37 °C, thus non-resistant starch was solubilized and hydrolysed into D-glucose and maltose.
171 The reaction was terminated by adjusting pH to 8.2 and heating to 95 °C to inactivate both PAA and
172 AMG. Proteins in the samples were denaturated and digested with protease. After this step soluble,
173 insoluble and accordingly total dietary fibre contents were determined as described in detail in the
174 Megazyme assay procedure.

175 **2.9. Total phenolic content**

176 The extractions and measurements of phenolics were made according to methods for extraction and
177 analyses described by Howard, Clark & Brownmiller (2003) and Barnes, Nguyen, Shen & Schug (2009),
178 with some modifications. Frozen extruded snacks consisting of rye flour with and without added bilberry
179 powders were freeze-dried and ground to smallest possible particle size using a mortar. Triplicate
180 samples (0.2±0.015 g) were extracted in screw-cap tubes with methanol/water/Triflouracetic acid
181 (70:30:1 (v/v)). The samples were vortexed for 15 s followed by sonication for 2x5 min and incubation
182 for 30 min (60 °C, 100 rpm). After cooling on ice the tubes were vortexed again for 15 s and centrifuged
183 at 5000 g for 5 min at 4 °C. Supernatants were collected and the remaining pellets were re-dissolved in
184 5 ml extraction solution. After vortexing for 15 s and sonication (2x5 min) and centrifugation (5000 g,
185 5 min, 4 °C) the 2 supernatants were combined. The phenolic content of the extracts was determined
186 spectrophotometrically with Folin-Ciocalteu's reagent against a standard curve of gallic acid and
187 measuring absorbance at 765 nm² on a Safire plate reader (TECAN) with Magellan software. The results
188 are expressed in mg gallic acid equivalents in g of dry weight (mg GAE/g). The dry weight was
189 determined by duplicate measurements on a dry matter analysis scale.

190 **2.10. Consumer evaluation**

191 The 4 extruded samples containing bilberry powder were evaluated using a convenience consumer panel
192 of 15 participants, 3 men and 12 women between 20 and 60 years old recruited among colleagues
193 external to the project at Chalmers. This panel was used with the aim to perform a feasibility study,
194 answering the needs of early stages in a product development process. The low number of consumers
195 involved may not be used to draw conclusions from a representative statistical point of view, but to
196 provide initial insights on the perceived texture variations and palatability of the extruded samples. The
197 samples were coded with 3-digit random numbers and presented together with a score-card in a
198 randomized balanced order to each participant (MacFie, Bratchell, Greenhoff & Vallis, 1989). For each
199 sample, a 9-point hedonic rating scale (1=extremely bad, 5=neither good nor bad, 9=extremely good)
200 was first used to evaluate overall liking, appearance, taste and texture. Then, a Just-About-Right (JAR)
201 scale (Lawless & Heymann, 2010) was used to provide a subjective quantitative evaluation of specific
202 texture attributes: crispness, porosity, stickiness and hardness (1: Far from [crispy] enough, 5: Just about
203 right, 9: Far too [crispy]). Drinking water was provided for mouth rinsing between samples. All samples
204 were presented in blind condition, i.e. without any information about processing or ingredients content.

205 **2.11. Statistical methods**

206 Multiple comparison tests using Tukey's honest significant difference criterion was performed to assess
207 if there were any statistically significant differences between measurement data in Figure 1 and Table 1
208 & 2. A value of $p < 0.05$ was considered statistically significant. For the sensory results the data were
209 analyzed by means of analysis of variance (ANOVA) in The Unscrambler X 10.3 (CAMO Software AS,
210 Norway). The ANOVA model tested the main effects of factors drying process and bilberry powder
211 content on the consumer responses. As only 15 consumers joined the feasibility study, significance
212 testing in this case is very conservative. No significant effects were detected at a 5% level and one effect
213 was detected at a 10 % level. In order to report on favourable directions to follow in future product
214 development phases, focus will be made on reporting the largest size effects as well as results at a
215 significance level of 20 %.

216

217 **3. Results and Discussion**

218 **3.1. Characteristics of dried bilberry press cake**

219 Bilberry press cake qualified as a suitable raw material for drying and subsequent processing since the
220 skin of the berries had already been broken facilitating water removal, and due to low sugar levels after
221 juice separation which reduced stickiness of the berry material. Moisture content, water activity and
222 total phenolic content of the dried materials is presented in Table 1. HA drying of bilberry press cake at
223 40 °C resulted in the longest drying time (360 min) while for MWA drying the drying time was 215
224 min. Hence, MWA drying enabled a 40 % reduction in drying time compared to HA drying. While
225 HA drying consists of heating from the outside towards the core by convection and conduction,
226 microwave drying is based on internal temperature rise due to electromagnetic heating. In the present
227 study, MWA drying was used, which is a combination of the two drying techniques. This resulted in
228 more efficient drying than HA drying alone, which reduced the drying time. Also, the additional internal
229 drying achieved using microwaves may have influenced the microstructure of the berry material. After
230 milling, there was an indication that the MWA dried material contained a larger fraction of small
231 particles than the HA dried material (Fig. 1), which may be due to structural differences between the
232 two materials. The total phenolic content decreased significantly during drying, to a similar extent for
233 both drying techniques. Although the MWA drying reduced the total drying time, the final content of
234 total phenolics was similar in both materials. This may be due to that heat sensitive phenolics were lost
235 early in the drying process, and prolonged drying (as in the case of HA drying) did not cause further
236 polyphenol losses. However, thermal degradation of polyphenols is in general more common at higher
237 temperatures, as demonstrated by Michalska, Wojdylo, Lech, Lysiak & Figiel (2017) for black current
238 pomace powder where drying at temperatures ranging from 50-90 °C resulted in a linear decrease in
239 total phenolics but with minor effects at 50 °C. Blueberry polyphenol oxidase, which in the presence of
240 oxygen causes degradation of major polyphenolic compounds has been reported to show activity over a
241 wide temperature range (25-65 °C). In the current study drying at 40°C may have enabled enzymatic

242 degradation during the initial drying steps (Siddiq & Dolan, 2017). Subsequent milling of the dried press
243 cakes did not affect either the moisture content or the total phenolic content.

244 **3.2.Characteristics of bilberry-wholegrain rye extrudates**

245 The addition of bilberry press cake powders to the wholegrain rye based formulation caused a significant
246 decrease in the degree of expansion of the wholegrain rye extrudates, indicated by an increase in the
247 specific density from 198 kg/m³ (wholegrain rye) to 245 and 335 kg/ m³, respectively for 10% and 25%
248 bilberry press cake addition (Fig. 2, Table 2). The dietary fibre (DF) content of extrudates was 23.7
249 g/100 g (8.5 g/100 g soluble, 15.2 g/100 g insoluble), 25.8 g/100 g (9.1 g/100 g soluble, 16.7 g/100 g
250 insoluble), and 27.9 g/100 g (9.4 g/100 g soluble, 18.5 g/100 g insoluble), respectively for wholegrain
251 rye, 10 % and 25 % bilberry press cake added samples. Addition of bilberry press cake powder to
252 wholegrain rye flour significantly increased the insoluble DF, which went through only minor structural
253 changes during extrusion and acted mainly as filler particles that led to structural anisotropy (Fig. 2). A
254 similar phenomenon was observed in the literature when other fruit press cakes (eg. apple, blackcurrant)
255 were utilized as DF sources in starch based extrudates (Karkle, Alavi & Dogan, 2012; Mäkilä et al.,
256 2014; O'shea, Arendt & Gallagher, 2014; Wang et al., 2017). Addition of DF resulted in inferior
257 structural and textural responses in extrudates as increasing the DF content led to lower expansion, high
258 density, less crispy but rather hard products (Alam et al., 2014; Alam et al., 2017). More than 5-10 g/100
259 g cherry or grape press cake addition levels caused adverse structural and textural effects (Altan,
260 McCarthy & Maskan, 2008; Wang et al., 2017). Insoluble DF was shown to alter the glass transition of
261 the melt due to high hydrophilicity and increased water absorption (O'shea et al., 2014). Specific
262 mechanical energy refers to the level of energy per mass unit that is transferred to the material by
263 mechanical input during extrusion. The SME value was 0.27, 0.17 and 0.13 kWh/g for wholegrain rye
264 flour, 10 % and 25 % bilberry press cake supplemented rye flour, respectively. The gradual decrease in
265 SME values might be related to the gradual increase in moisture content (from 11 to 12.5 g/100 g) with
266 the increase in bilberry press cake addition amount (from 0 to 25 %) but also with the gradual reduction
267 in starch content whilst increasing the bilberry press cake and in turn insoluble dietary fibre content.
268 Extrudate expansion is strongly influenced by biopolymer interactions and melt rheology (Sozer &

269 Poutanen, 2013). In order to achieve a well-expanded extruded matrix, the shear viscosity of the melt
270 should be low enough for growth of air cells and further expansion, but high enough to inhibit collapse
271 of air cells (Pai, Blake, Hamaker & Campanella, 2009). The incorporation of inert insoluble particles
272 such as the IDF in bilberry press cake might have reduced the starch viscosity at constant melt
273 temperature. This might led to reduced mechanical starch transformation in the extruder due to reduced
274 SME which will further result in dense, hard and less crispy textures.

275
276 The addition of bilberry press cake powder increased both the hardness and crispiness work regardless
277 of addition level. The crispiness index was the highest for 25 % HA bilberry press cake powder (Table
278 2). Differences in microstructure between HA and MWAHA dried press cake may have affected the melt
279 properties during extrusion processing. The consumer evaluation reports variations in texture
280 corresponding to the above physical measurements (Fig. 3). On average, extruded products with addition
281 of 10 % bilberry press cake powder were described to have a more enjoyable texture (mean score 6.2
282 on the 9-point hedonic scale) than products with addition of 25 % bilberry press cake powder (mean
283 score 5.3) (Fig. 3a). More specifically, 10 % addition of bilberry press cake powder resulted in
284 properties of porosity and hardness closer to the consumers' ideal point on average. These samples
285 presented a more porous (mean JAR score 5.5; $p=0.20$), less crispy (mean JAR score 5.7, $p=0.08$) and
286 less hard (mean JAR score 4.7; $p=0.13$) texture than for the extrudates with 25 % addition of bilberry
287 powder (porosity mean JAR score: 4.1, i.e. somewhat not porous enough; crispy mean JAR score: 5.4;
288 hardness mean JAR score: 5.9, i.e. somewhat too hard) (Fig. 3b). Consequently, the decrease in degree
289 of expansion and increase in density, which was proportional to bilberry press cake powder addition,
290 was perceived by the consumers as decreased porosity and increased hardness. Attribute stickiness
291 showed very little variation between samples, with an overall mean of 5.6 on the JAR scale (Fig 3b).
292 Visual appearance and taste were moderately acceptable for all extrudates with average scores around
293 the hedonic scale's mid-point (Fig. 3a). However, the extrudates from HA process scored slightly better
294 in overall liking (mean score: 5.8; $p=0.16$), than did the extrudates with MWAHA process (mean score:
295 5.2) (Fig. 3a). HA drying also tended to be preferred to MWAHA drying in terms of visual appearance
296 ($p=0.17$) and to lead to lower crispness perception ($p=0.11$). All in all, the bilberry press cake enriched

297 extrudates were considered moderately palatable by the subjects and the concept of a healthier cereal
298 based snack was regarded as positive. Due to the very small size of the panel, the directions of
299 preferences reported here are only indicative and supportive of the feasibility study. Further consumer
300 tests targeted at the market population will be necessary in future stages of the product development
301 process. At this stage, the relationship between the panel's evaluations and the processing parameters
302 are valuable inputs for further texture management of puffed extrudates containing berry materials.
303 Lipids in berry seeds may cause problems with oxidation in products, which could be more prominent
304 in the extrudates with high bilberry press cake addition levels. However, no negative effects on taste or
305 overall liking were seen for extrudates with 25 % addition compared to 10 % addition. The press cake
306 contained large amounts of seeds. Some of these seeds were broken during milling, but many stayed
307 intact (visual observation). Although extrusion processing of bilberry press cake caused a significant
308 reduction in the total phenolics content; it also caused a dramatic increase in total phenolics of puffed
309 extrudates in proportion to the addition level (Tables 1 & 2). The overall decrease in total phenolics
310 might be a result of decarboxylation due to combined high temperature and moisture during extrusion
311 (Brennan, Brennan, Derbyshire & Tiwari, 2011). The total phenolic content was slightly higher in
312 extruded snacks with MWAH dried bilberry powders compared with snacks containing HA dried
313 bilberry powders ($p < 0.05$). The observed differences in total phenolic content may be related to different
314 extractability of phenolic compounds due to microstructural differences between HA and MWAH dried
315 press cake.

316

317

318 **4. Conclusions**

319 Mild drying and extrusion processing of side streams from berry juice production enables retention of
320 valuable compounds in the food chain and reduced waste production. This study showed that powder of
321 bilberry press cake could be incorporated in cereal based extruded snacks with acceptable appearance,
322 taste and texture as well as enhanced phenolic content. This is a promising way to provide healthy low-
323 fat snack products rich in dietary fibres and polyphenols. Different drying techniques implied a

324 difference in processing time (40% reduced drying time with MWA drying). However, the retention
325 of total phenolics and physical characteristics were similar for snacks extruded from bilberry powders
326 produced with different drying techniques. Further studies of the combination of drying techniques and
327 extrusion on the sensory characteristics and health-beneficial compounds remaining in bilberry press
328 residues and extrudates are needed.

329

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446 texture. *Food Chemistry* 212, 671-680.

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451 Figure captions

452 Figure 1. Particle size distribution of the dried and milled bilberry press cake. No values were
453 significantly different ($p < 0.05$) based on Tukey's test.

454

455 Figure 2. Stereomicroscope images of radial sections of the extrudates. Reference wholegrain rye flour
456 extrudate with no added press cake (WG); 10 % hot air and microwave assisted hot air dried bilberry
457 press cake added extrudate (10HA and 10MWA, respectively); 25 % hot air and microwave assisted
458 hot air dried bilberry press cake added extrudate (25HA and 25MWA, respectively).

459 Figure 3. Consumer evaluation ($n=15$) of rye/bilberry extrudates. (a) Hedonic evaluation. A value of 9
460 corresponds to "extremely good". (b) Subjective quantitative evaluation. A value of 5 corresponds to
461 "just about right".

462

463 Table 1. Characteristics of the bilberry press cake (mean \pm standard deviation). Values followed by the
 464 same letter in the same line were not significantly different ($p < 0.05$) based on Tukey's test.
 465

Bilberry material characteristics	Moisture content (g/100 g)	Water activity	Total phenolic content (mg/g DW)
Press cake	75.6 \pm 0.5 ^a	-	216.1 ^a \pm 5.3
Hot air drying, not milled	18.9 \pm 2.1 ^b	-	60.4 ^b \pm 2.6
Microwave hot air drying, not milled	17.8 \pm 1.0 ^b	-	58.4 ^b \pm 0.3
Hot air drying, milled	16.9 \pm 0.1 ^b	0.757 ^a \pm 0.003	61.9 ^b \pm 0.5
Microwave hot air drying, milled	17.0 \pm 0.2 ^b	0.755 ^a \pm 0.004	62.0 ^b \pm 2.8

466

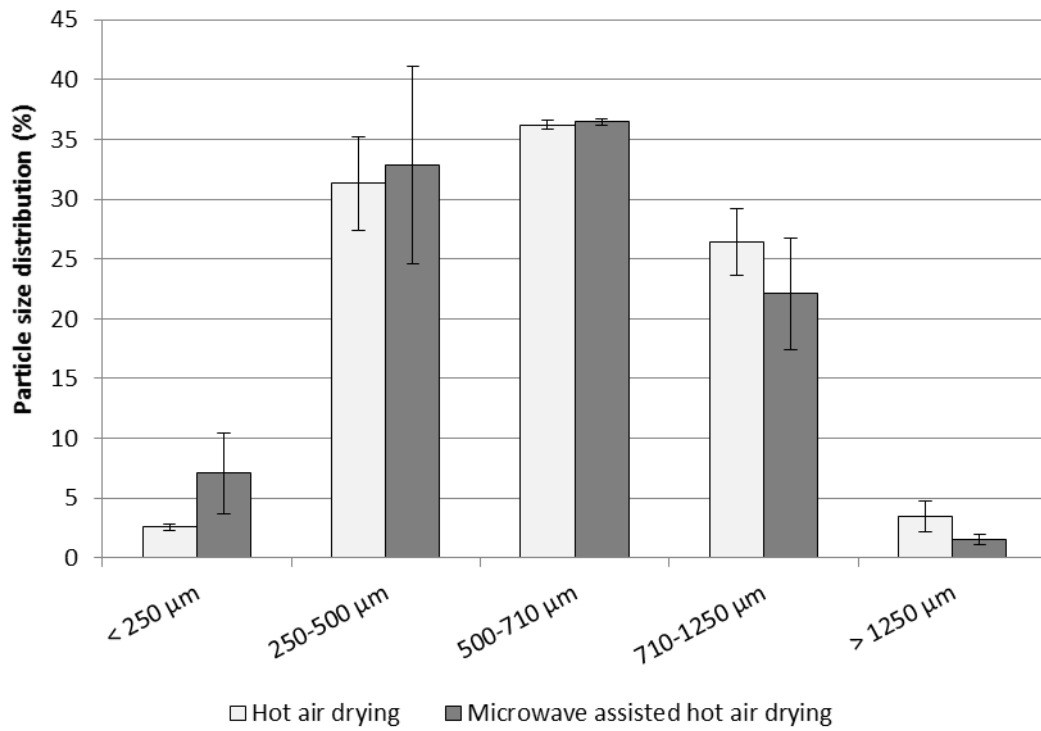
467 Table 2. Characteristics of the extruded snacks (mean \pm standard deviation). Values followed by the
 468 same letter in the same line were not significantly different ($p < 0.05$) based on Tukey's test.
 469
 470

Extruded snack characteristics	Rye	Rye + 10 % Hot air dried bilberry powder	Rye + 10 % Microwave assisted hot air dried bilberry powder	Rye + 25 % Hot air dried bilberry powder	Rye + 25 % Microwave assisted hot air dried bilberry powder
Degree of expansion (%)	360 \pm 12 ^c	295 \pm 8 ^b	298 \pm 8 ^b	246 \pm 4 ^a	246 \pm 7 ^a
Specific density (kg/m³)	198 \pm 9 ^a	246 \pm 12 ^{bc}	245 \pm 14 ^c	329 \pm 12 ^{ab}	335 \pm 16 ^{bc}
Hardness (N)	48 \pm 4 ^a	53 \pm 2 ^{bc}	57 \pm 5 ^c	51 \pm 3 ^{ab}	55 \pm 7 ^{bc}
Crispness work (N/mm)	2.5 \pm 0.3 ^a	3.0 \pm 0.5 ^{bc}	3.0 \pm 0.3 ^{bc}	2.8 \pm 0.5 ^{ab}	3.5 \pm 0.5 ^c
Crispness index	1.7 \pm 0 $\times 10^{-3b}$	1.3 \pm 0 $\times 10^{-3a}$	1.2 \pm 0 $\times 10^{-3a}$	2.5 \pm 0 $\times 10^{-3c}$	1.7 \pm 0 $\times 10^{-3b}$
Total phenolic content (mg/g DW)	0.59 \pm 0.00 ^c	3.50 \pm 0.05 ^d	3.89 \pm 0.07 ^c	7.40 \pm 0.20 ^b	7.82 \pm 0.08 ^a

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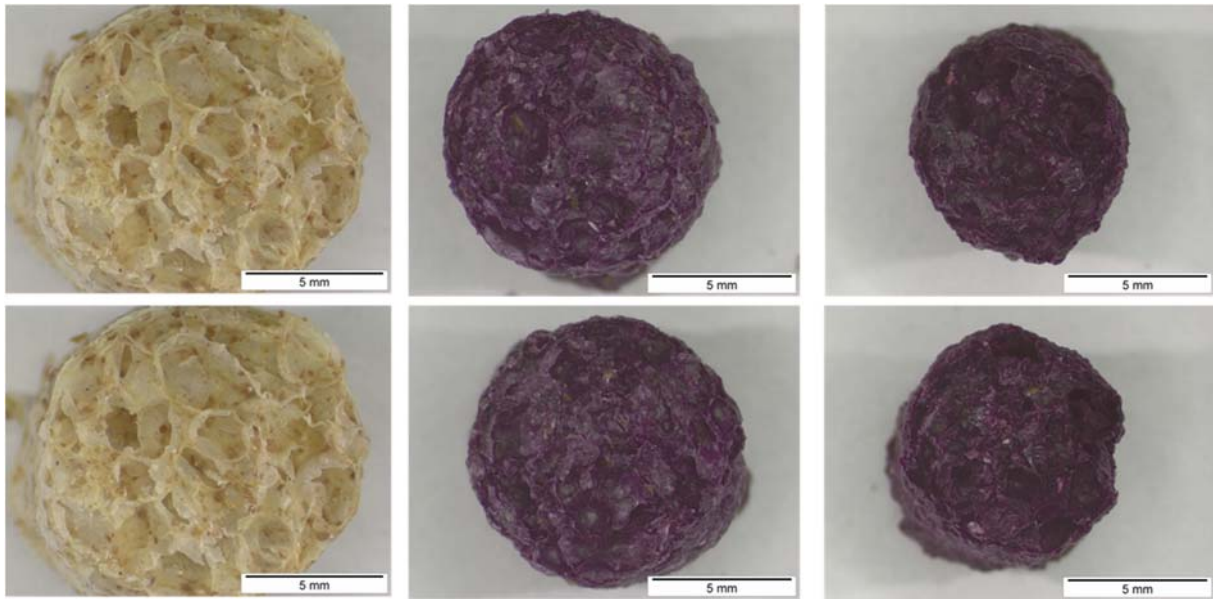


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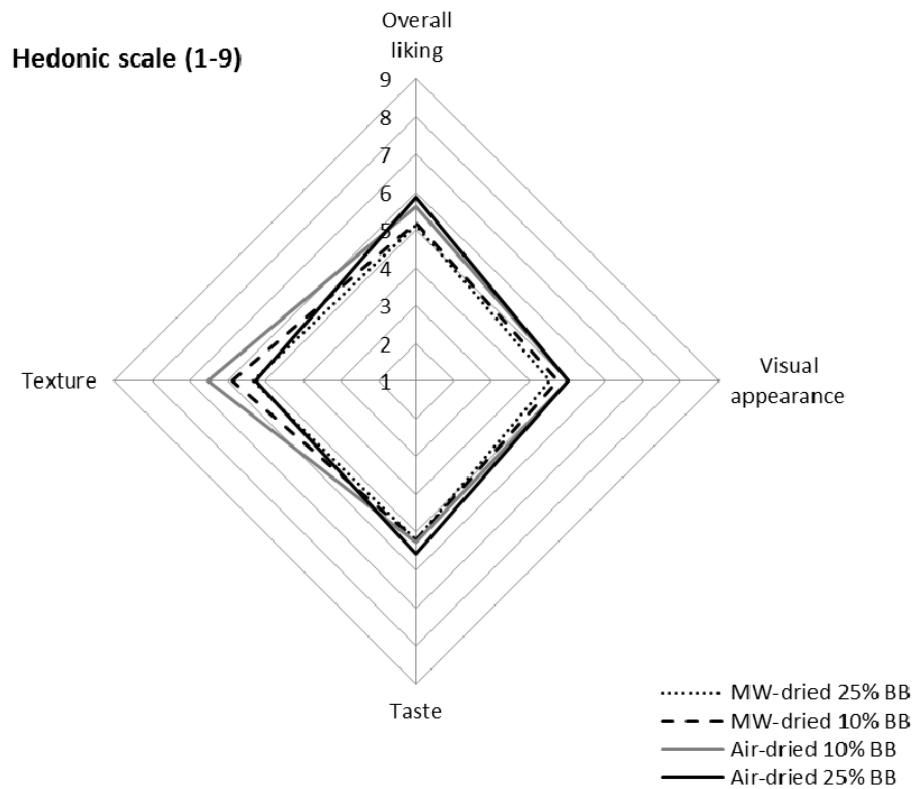
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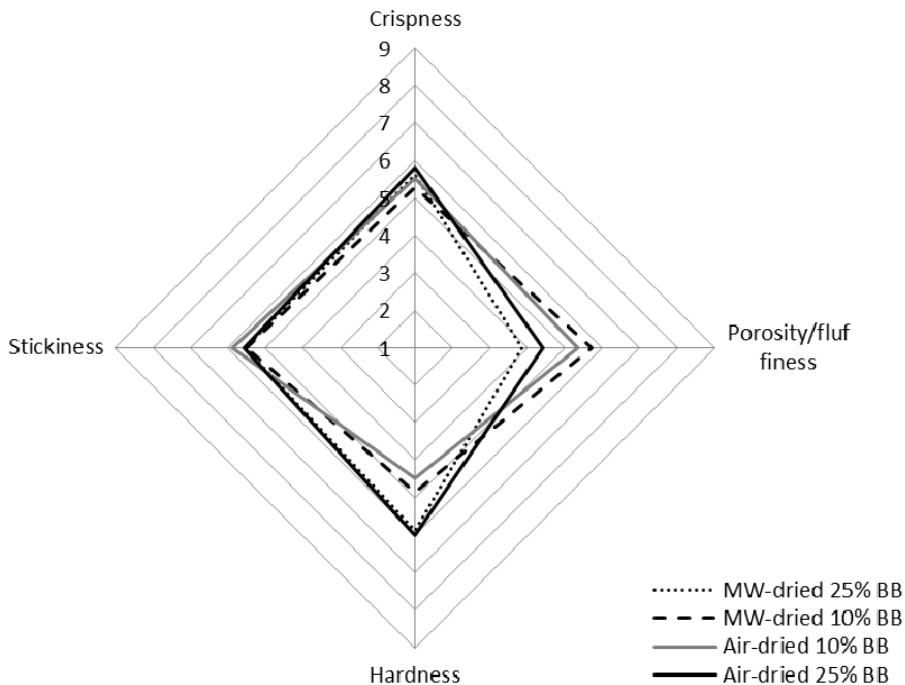
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484



Texture attributes evaluated by just-about-right scale



485

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